



Radiation Pattern of a Circularly Polarized Microstrip Short Backfire Antenna

Kawa Abdoula^{1*}

¹*Department of Communication Engineering, Technical University of Varna, Studentska Str. 1, 9010 Varna, Bulgaria.*

Author's contribution

The sole author designed, analyzed and interpreted and prepared the manuscript.

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ABSTRACT

A circularly polarized microstrip short backfire antenna (CPMSBA) with one ring corrugated rim, using aperture coupled feed method is proposed in this paper. The antenna is designed to operate in KU-band. The simulation results verify the circular polarization. The impedance bandwidth is 0.83 GHz. The CP antenna provides good radiation pattern over the whole frequency range. The axial ratio bandwidth bwAR is 2.96%, the gain is 9.79 dBi, directivity is 10.17 dBi and radiation efficiency is 91.62%. The antenna has a compact structure, high electrical and mechanical characteristics, it can be used as a single antenna or as an element of microstrip antenna arrays with various applications in the various communication systems.

Keywords: Radiation pattern; aperture coupled microstrip antenna; back radiation; circularly polarized microstrip antenna with one ring; microstrip short backfire antenna.

1. INTRODUCTION

Recently there has been a growing demand of microwaves in various applications resulting in

an interest to improve antenna performances. Wireless communication systems and instruments like wireless local area networks (WLAN), cellular phones etc. require small size,

*Corresponding author: E-mail: Kawa1_abdoula@hotmail.com;

low cost, light weight antennas. The selection of microstrip antenna technology can fulfill these requirements [1-3]. Significant advances in the design of microstrip antennas have been presented over the last decades. Defected ground structure is one of the techniques used to reduce the antenna size [4]. Microstrip patch antennas suffer from several inherent disadvantages of this technology in its pure form, namely, they have small bandwidth and relatively poor radiations efficiency resulting from surface wave excitations and conductor and dielectric losses. Many specialized techniques have been developed to increase the bandwidth of a microstrip antenna. These include either using thick foam substrates along with aperture coupled feeds to avoid the probe reactance limitation, or using capacitive elements to compensate for the probe inductance. Even further increases may be achieved by using configurations that exhibit dual or multiple resonances, including stacked resonators or antennas surrounded by parasitically coupled elements. [5]. Microstrip Backfire Antenna can be used as single antenna can take the place of four or more microstrip radiating elements and provide overall thinning of an array. Circularly polarized antenna is employed to avoid power loss caused by Faraday polarization rotation in satellite communications. [6–9]. The microstrip antennas (MSAs) may be designed for circular polarizations by adjusting their physical dimensions to produce two degenerate orthogonal modes with in the cavity region. This in turn results in the radiation of two orthogonally polarized waves near the broadside direction. Thus, circularly polarized radiation is obtained when two orthogonal modes are excited with equal amplitude and in-phase quadrature [10].

2. RADIATIONS MECHANISM

The basic microstrip antenna is consisting of a radiating patch on one side of a dielectric substrate, which has a ground plane of the other side. The microstrip patch and the ground plane together form a resonant cavity (filled with the substrate material). The cavity is lossy, due not only to the material (conductor and dielectric) loss, but also to the (desirable) radiation into space [11].

In Fig. 1. The electromagnetic energy provides by the feed microstrip line passes through rectangular slot into the first resonator formed by patch element and the ground plane. After multiple reflections between the inner walls of the

first resonator, a part of this energy radiated directly into the space and other part of this electromagnetic energy penetrates via the short sides of the patch element to the second resonator, formed by the small reflector and ground plane. After multiple reflections between the inner walls of the second resonator, the electromagnetic energy radiated between the short sides of the small reflector and the rim in the broadside of the antenna. The rim reduces the back and side radiations of the proposed antenna.

3. DESCRIPTION OF THE ANTENNA

Fig. 1. shows the geometry of the aperture coupled microstrip short backfire antenna (ACMSBFA) The antenna consists of the following elements:

1. Screen
2. Screen Substrate
3. Feed line
4. Feed substrate
5. Ground (D2)
6. Rim
7. Rectangle Cross-Slot
8. Patch
9. Patch substrate
10. Small Reflector (D1)
11. Additional substrate.
12. Small reflector Substrate
13. Additional ring and five substrates as follows: additional substrate AS (Taconic TLX-7: $\epsilon_{rt} = 2.6$, $\tan \delta_t = 0.0019$); small reflector substrate SRS (Arlon AD 410: $\epsilon_{rq} = 4.1$, $\tan \delta_q = 0.0030$, the small reflector substrate is realized by two layers with standard thickness of 3.175 mm); patch substrate PS (Arlon AD 600: $\epsilon_{rp} = 6.15$, $\tan \delta_p = 0.0030$); feed substrate FS (Arlon AD 600: $\epsilon_{rf} = 6.15$, $\tan \delta_f = 0.0030$) and screen substrate SS (Taconic TLX-7: $\epsilon_{rs} = 2.6$, $\tan \delta_s = 0.0019$).

4. DESIGN OF THE ANTENNA

The linearly polarized (LP) antenna with aperture coupled method is chosen as a prototype, as it is allowing independent optimizations of the both parts of the antenna (feeding and radiations parts).

The transitions of LP to circularly polarization (CP) is done by creation a cross slot (insertions of the second slot Sl_2 orthogonal to the first slot Sl_1) and rotation of the microstrip feed line by 45 degrees around the cross slot. The values of the basic dimensions and constructive parameters were determined by optimizations procedure done by software package CST MWS 2010 and the results were verified with software package HFSS.

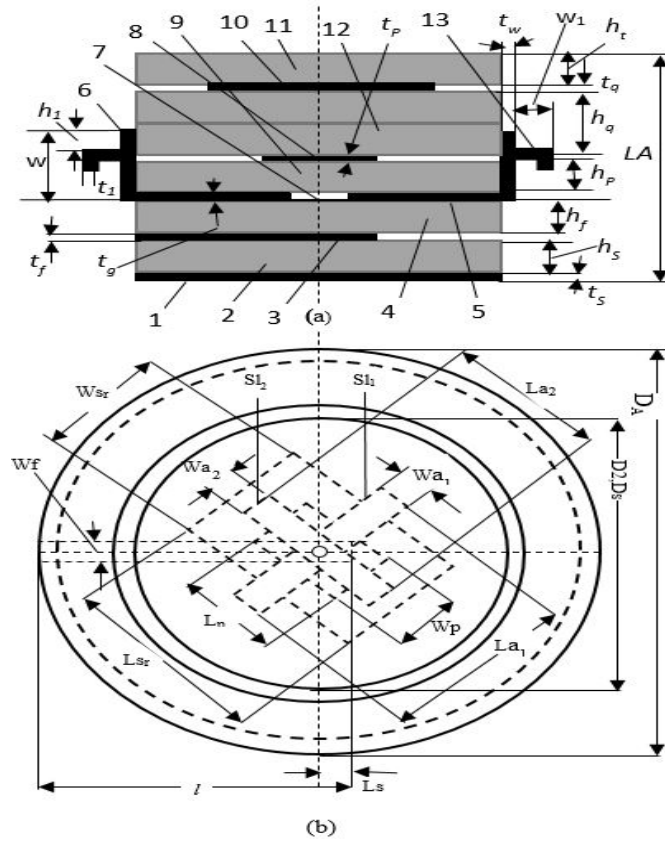


Fig. 1. Geometry of the antenna
(a) Cross section (b) Front view

14 of the dimensions and constructive such as patch width WP , patch length LP , cross slot average length La , patch size coefficient KP , cross slot size coefficient KS , slot 1 length $La1$, slot 1 width $Wa1$, slot 2 length $La2$, slot 2 width $Wa2$, small reflector length Lsr , small reflector size coefficient $K1$, small reflector width Wsr , ring width $W1$, and the matching stub length LS were used in the optimization.

Their number was reduced to 8 using the 6 interrelations to the $La1$, $La2$, $Wa1$, $Wa2$, WP and Wsr shown in Table 2. The rest of the parameters such as LP , $K1$, KP , KS , La , Ls , Ls , and $W1$ are optimized independently.

These parameters are investigated in the frequency range 10 GHz to 13.5 GHz. The optimum values of these eight parameters are found by several iterations as shown in the Table 2.

The dimensions of the proposed CP antenna are listed in the Table 1, the optimized parameters of

the antenna structure are listed in Table 2, and the electrical parameters of the CP antenna are shown in the Table 3.

5. SIMULATIONS RESULTS

The simulations of the proposed antenna are carried out by software package CST MWS 2010 and the results were verified with software package HFSS. The parametric analysis was completed and published [12].

Fig. 2a, b and c Shows the radiation pattern at frequency 11.62 GHz, $\varphi = 0$, $\varphi = 45$ and $\varphi = 90$ degree. Co-polarization radiation pattern or right hand circularly polarization (RHCP) with red line and cross-polarization radiation pattern or left hand circularly polarization (LHCP) with blue dashed. The radiation pattern of the antenna illustrates the distribution of radiated power in the space. it seems from the figure that the CP antenna provides good and stable radiation pattern over the whole frequency range.

Table 1. Dimensions of the antenna

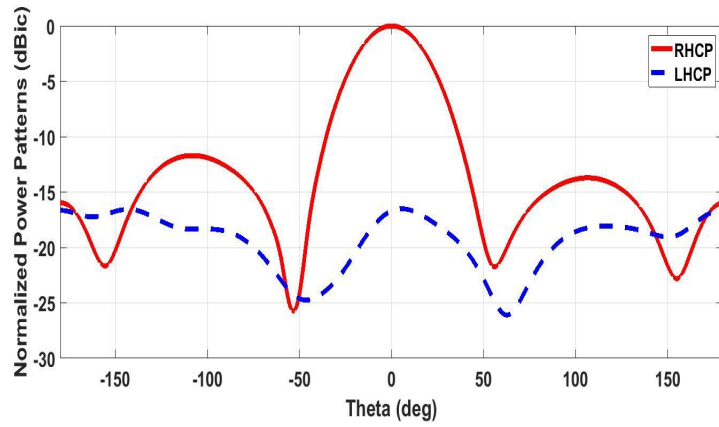
| Dimensions[mm] | Description | |
|-----------------|-------------|---|
| D2 | 24 | Big Reflectors inner diameter |
| tg | 0.0175 | Big reflector& ground thickness |
| L | 13.155 | Antenna length |
| Wsr | 3.30 | Small reflector width |
| W | 7.6825 | Rim width |
| tt | 0.035 | Small reflector thickness |
| tw | 0.5 | Rim thickness |
| Wp | 2.38 | Patch width |
| tp | 0.035 | Patch thickness |
| Wa ₁ | 0.45 | Slot1 width=0.1 La1 |
| Wa ₂ | 0.40 | Slot2 width=0.1 La2 |
| l | 11.9 | Microstrip feed line length |
| Ls | 1.0 | Stub length |
| Wf | 0.98 | Microstrip feed line width |
| tf | 0.0175 | Microstrip feed line thickness |
| Ds | 24 | Screen diameter |
| ts | 0.035 | Screen thickness |
| ht | 1.58 | Additional substrate thickness |
| hq | 6.35 | Small reflector substrate thickness |
| hp | 1.27 | Patch substrate thickness |
| hf | 0.635 | Feed substrate thickness |
| hs | 3.175 | Screen substrate thickness |
| t1 | 0.5 | Ring thickness |
| h1 | 0.4 | Distance between the upper edge of the peripheral screen and the upper edge of the ring |

Table 2. Optimized parameters of the antenna structure

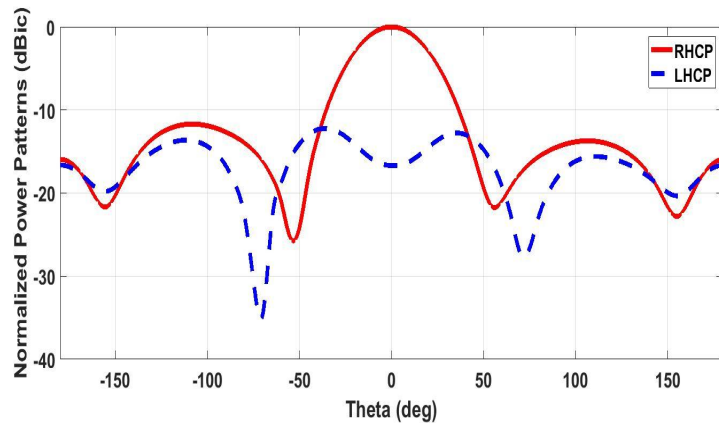
| Name | Value[mm] | Description |
|------|--------------------|-------------------------------|
| Lp | 2.7 | Patch length |
| K1 | 1.08 | Small reflector ratio Lsr/Wsr |
| Kp | 1.06 | Patch Ratio Lp/Wp |
| Ks | 1.10 | Slot Ratio La1/La2 |
| La | 4.1 | Slot length |
| La1 | $(2*La*Ks)/(Ks+1)$ | Aperture 1 length |
| La2 | $2*La/(Ks+1)$ | Aperture 2 length |
| Ls | 0.9 | Stub length |
| Lsr | 4.1 | Small reflector length |
| Wa1 | La1/10 | Aperture 1 width |
| Wa2 | La2/10 | Aperture 2 width |
| Wp | Lp/Kp | Patch width |
| Wsr | Lsr/K1 | Small reflector width |
| W1 | 3.8 | Ring width |

Table 3. Electrical parameters of the antenna

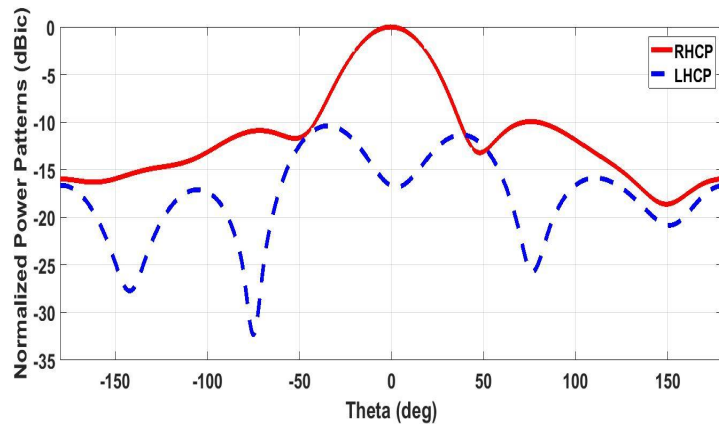
| | | | |
|--------------------------------|-----------|----------------------------------|-----------|
| Impedance bandwidth | | Central frequency f_{0AR} | 11.79 GHz |
| Minimum frequency f_{min} | 11.41 GHz | Frequency bandwidth BWAR | 0.35 GHz |
| Maximum frequency f_{max} | 12.24 GHz | Relative bandwidth bw_{AR} , % | 2.96% |
| Central frequency f_0 | 11.82 GHz | G_{min} dBi | 8.38 dBi |
| Relative bandwidth bw , % | 7.02% | G_{max} dBi | 9.79 dBi |
| Frequency bandwidth BW | 0.83 GHz | BR_{min} dB | -16.37 dB |
| Axial Ratio bandwidth | | BR_{max} dB | -21.23 dB |
| Minimum frequency $f_{min AR}$ | 11.62 GHz | Efficiency $\eta_{max\%}$ | 91.62% |
| Maximum frequency $f_{max AR}$ | 11.97 GHz | Directivity D_{max} dBi | 10.17 dBi |



(a)



(b)

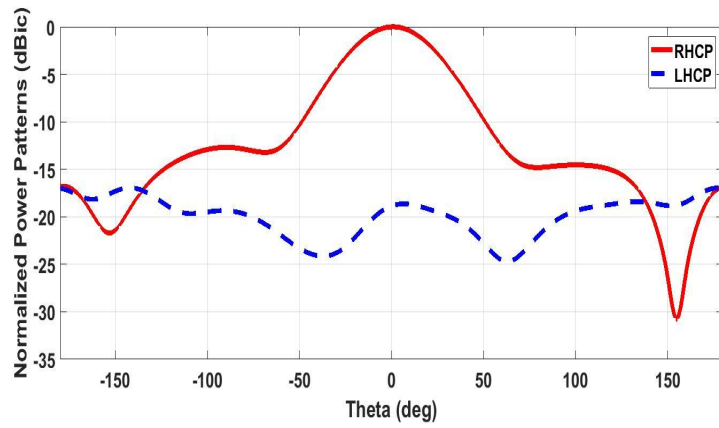


(c)

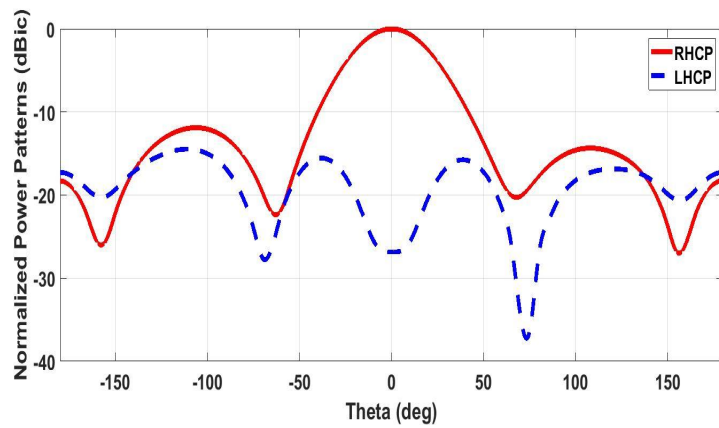
Fig. 2. Radiation pattern of the antenna at frequency 11.62 GHz, (a) $\varphi = 0$ degree, (b) $\varphi = 45$ degree, (c) $\varphi = 90$ degree, RHCP with red line and LHCP with blue dashed

Fig. 3.a, b and c shows the radiation pattern at frequency 11.79 GHz, $\varphi = 0$, $\varphi = 45$ and $\varphi = 90$ degree RHCP with red line and LHCP with blue dashed.

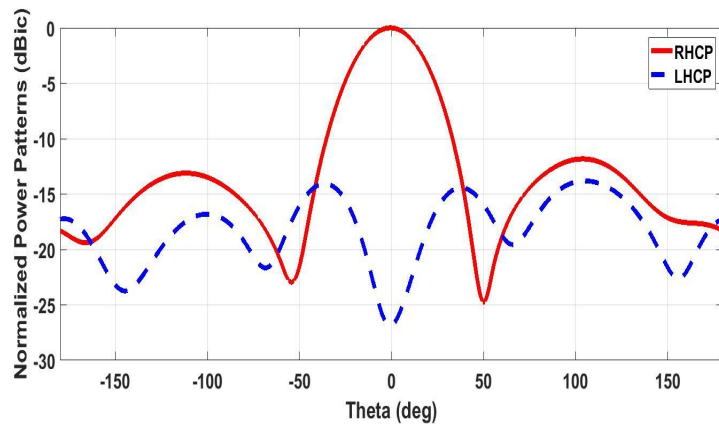
Fig. 4.a, b and c shows the radiation pattern at degree. RHCP with red line and LHCP with blue dashed frequency 11.97 GHz, $\varphi = 0$, $\varphi = 45$ and $\varphi = 90$ dashed.



(a)

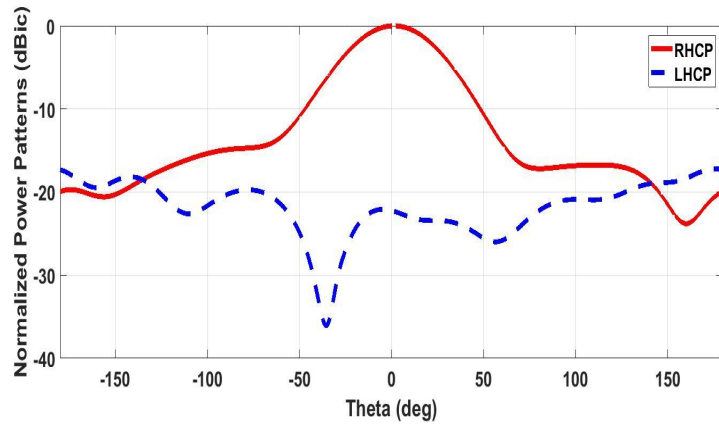


(b)

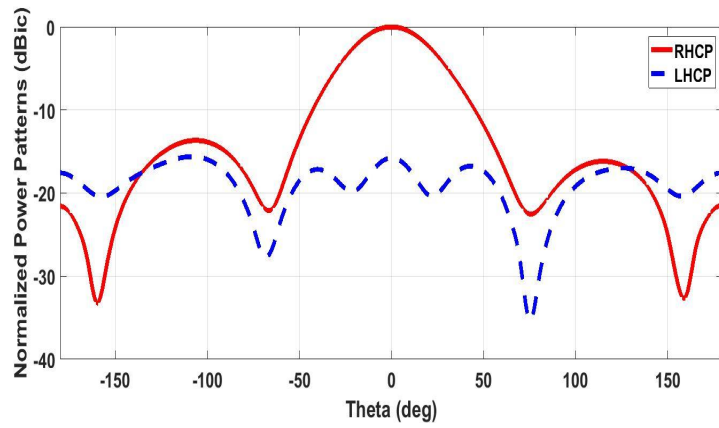


(c)

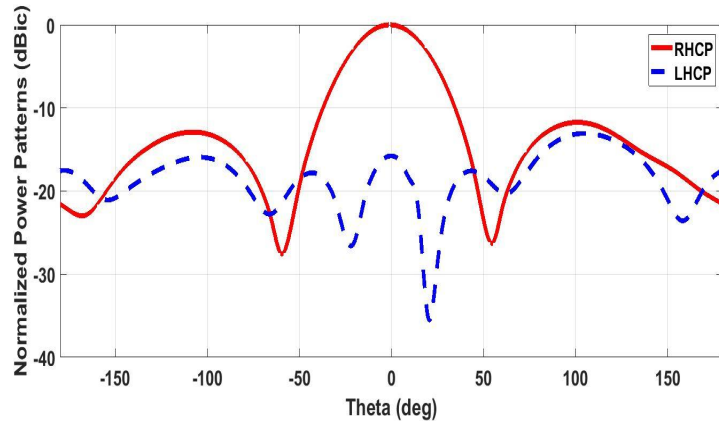
Fig. 3. Radiation pattern of the antenna at frequency 11.79 GHz, (a) $\varphi = 0$ degree, (b) $\varphi = 45$ degree, (c) $\varphi = 90$ degree, RHCP with red line and LHCP with blue dashed



(a)



(b)



(c)

Fig. 4. Radiation pattern of the antenna at frequency 11.97 GHz, (a) $\varphi=0$ degree, (b) $\varphi=45$ degree, (c) $\varphi=90$ degree, RHCP with red line and LHCP with blue dashed

Fig. 5. Shows comparisons of the co-polarizations (RHCP) at frequency 11.79 GHz, $\varphi=45$ degree with two different software's CST

MWS 2010 and HFSS, the both curves for RHCP have similar behaviors which indicated a good agreement of the obtained simulated results.

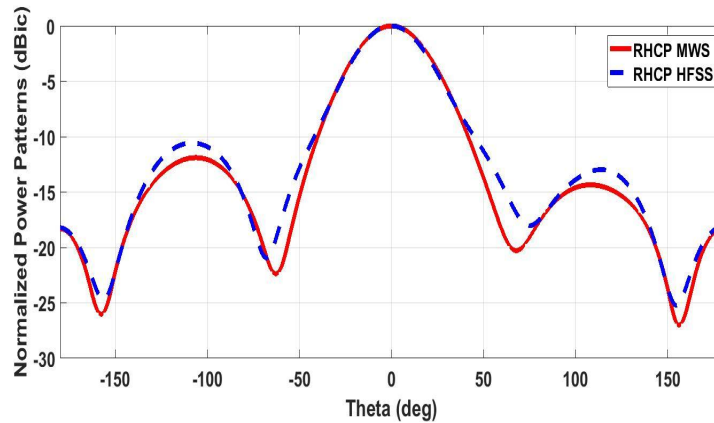


Fig. 5. Co-polarization (RHCP) of the antenna at frequency 11.79 GHz, $\phi = 45$ degree, MWS red line, HFSS blue dashed

6. DISCUSSION AND NUMERICAL RESULTS

In this study an aperture coupled microstrip short backfire antenna was designed and investigated. The following features of the proposed antenna design need discussion.

6.1 Advantage of the Antenna

The impedance bandwidth of the CP antenna bw_{S11} is 7% while its polarization bandwidth bw_{AR} is equal to 2.96%, this is good bw_{AR} bandwidth compared with the conventional microstrip antenna. The bandwidth enhancement in this case is due to the type of chosen feed, suitable choice of the values of substrate dielectric constants, thickness, optimization of antenna dimension and insertion of two resonances in the antenna impedance characteristics. The first of these resonance (the patch resonances) is at lower frequency while the second resonance (the backfire resonance) is at higher frequency.

The CP antenna gain ranges from 8.38 dBic to 9.79 dBic within the antenna bandwidth, at the central frequency $f_0 = 11.795$ GHz, the antenna has gain $G_0 = 9.6$ dBic, radiation efficiency $\eta_{eff} = 91.2\%$. The presence of corrugated rim improves the antenna gain by approximately 0.5 dBic compared to the antenna with conventional rim.

The back-radiation level of the CP antenna varies between -16 dB and -21 dB across the antenna bandwidth. The basic contribution to this good results is due to the presences of the screen and rim.

The antenna construction is compact, robust and with a low volume. The volume and aperture area of the antenna for example are 3 times less than the corresponding dimensions of the CP SBFA with an air cavity.

6.2 Disadvantage of the Antenna

The antenna gain is lower compared to the conventional CP SBFA with an air cavity due to the reduced dimension.

7. CONCLUSION

A broadband circularly polarized aperture coupled microstrip short backfire antenna with one ring corrugated rim has been designed and numerically investigated. The bandwidth widening of the antenna is achieved by use of two resonance: a patch resonance and a backfire resonance, it has maximum gain 9.79 dBi, maximum back radiation $BR_{max} = -21.23$, maximum efficiency 91.62% and axial ratio bandwidth is 2.96%, this is good bandwidth compared with conventional microstrip antenna. The antenna is designed to operate within KU-band. The designed antenna has a simple and compact construction and high mechanical and electrical characteristics; it can be used as a single antenna or as an element of microstrip antenna arrays with various applications, in the various communication systems, including radar, mobile communications, satellite communications and wireless local area networks.

COMPETING INTERESTS

Author has declared that no competing interests exist.

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